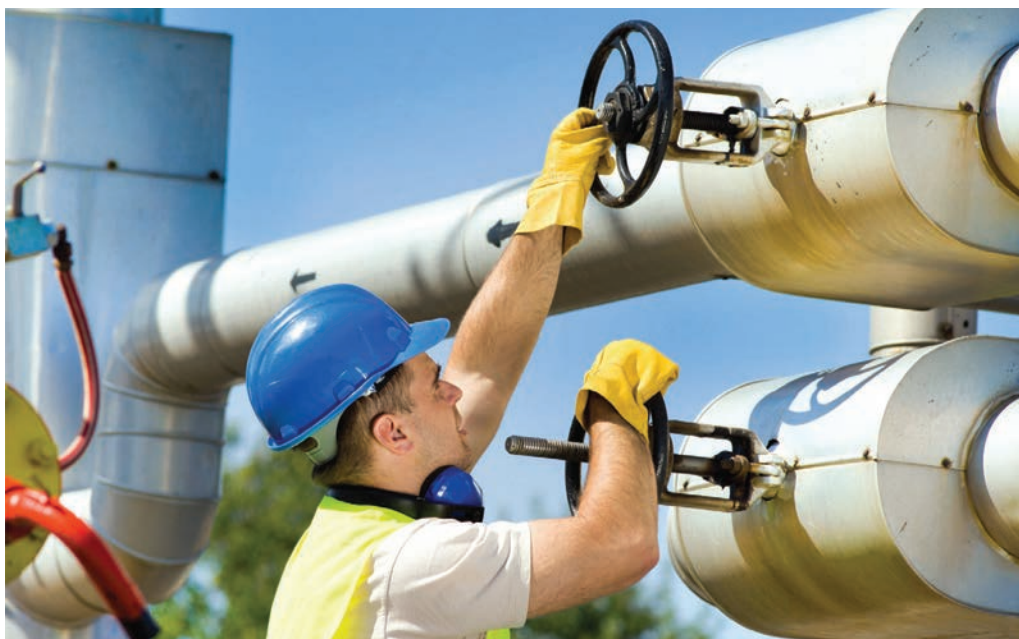


# Fitness for service

Fitness for service (FFS) encompasses various methodologies to evaluate cracks in equipment. These methodologies offer guidance in evaluating defects and deciding the safe course of action. This article will explore FFS methodologies and learn how they can be used in valves.

By Davi Sampaio Correia



**B**adak LNG is one of the largest natural gas liquefaction plants in the world, located in Bontang, Indonesia. There are eight process trains - capable of producing 22.5 million metric tons per annum of LNG - using steam turbines for driving power generation and refrigeration compressors.

On January 27, 2011, a routine inspection detected several cracks on a 24" #600 gate valve located on a steam line. There was no replacement valve available and depressurizing the adjacent piping would require shutting down a sizable portion of the plant. Pressure vessels for the process industry, including valves, are designed according to well-established ASME and API codes and standards. In truth, these standards provide rules not only for design, but also for fabrication, inspection, and testing of new equipment. The keyword here is new. Once flaws and damages start to appear, the original design documents offer little to no guidance on how to proceed.

## Multidisciplinary

In-service equipment will degrade; sometimes predictably, sometimes unpredictably. The former may be caused by a reduction in the corrosion-allowance extra-thickness due to an expected process; the latter may be a moss on the side of a pressure vessel caused by a lifting accident. Whatever the reason, industrial plants have to assess damages and decide if it is safe to continue operation once the equipment no longer complies with the original design assumptions.

Fitness for service (FFS) is a collection of techniques that were developed to provide guidance when dealing with flaws and damages in operating equipment. It often requires a multidisciplinary team, drawing

people from three technology areas: inspection, materials, and mechanical, as seen in Figure 1. Once the assessment has been made, there are four possible options the operator can consider: maintain operation as-is, maintain operation under restricted conditions, repair, or replace. It is worth mentioning that an FFS assessment is also useful for estimating remaining life, planning future inspections, and allocating financial provisions for future replacement, should the equipment be decommissioned.

There are many procedures and standards related to FFS evaluation, depending on geographic location, type of failure, industry, legislation, and personal preference. Across the Atlantic, for example, the British may use the BS7910<sup>2</sup>, the French the RCC-MR<sup>3</sup> or both could use the FITNET procedure<sup>4</sup>. In the United States, the scene is clearer: there are basically two options. One is the API 579<sup>7</sup> and its example manual<sup>8</sup> for the industry in general; and the ASME XI<sup>9</sup> for the nuclear industry. Since the API 579 is the standard with more widespread use, it is important to understand its function.

## The API 579: Overview

The API 579 defines an FFS assessment as, "A methodology whereby flaws or a damage state in a component is evaluated in order to determine the adequacy of the component for continued operation<sup>7</sup>." The FFS rules laid out in the API 579 are based on quantitative analysis of in-service flaws, but the principles can also be used to evaluate fabrication flaws.

There is no specific qualification process or certification prior that one can apply to the FFS methodologies, the only provision is that, "The level or amount of education and experience of all

### About the author

Davi Correia is a Senior Mechanical Engineer who has worked at a major Brazil-based oil company for the last 15 years. Correia is part of multi-disciplinary team that provides technical support for topside piping and equipment of production platforms. During this period, he began to work with materials and corrosion, and later moved to piping and accessories technology, where he has become one of the lead technical advisors on valve issues. Correia was part of the task force that revised the IOGP S-562 standard, and wrote the S-611 standard. Correia has a master's and a doctor's degree in welding by the Universidade Federal de Uberlandia.



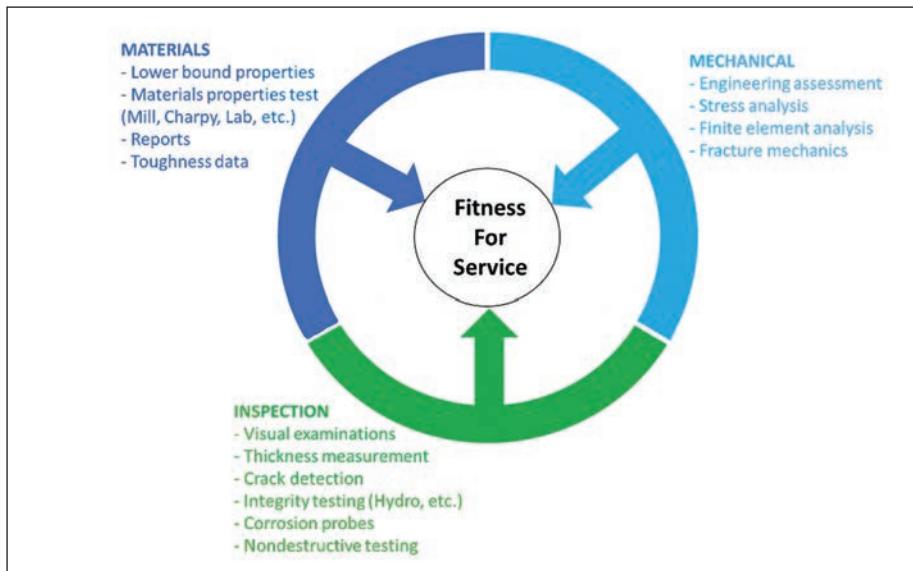


Figure 1: Technology triad required for fitness-for-service assessment.<sup>1</sup>

participants shall be commensurate with the complexity, rigor, requirements and significance of the overall assessment<sup>7</sup>.”

The API 579 has eleven assessment procedures, organized by type of discontinuity or damage mechanism, as summarized in Table 1. The standard also contains a series of annexes with complimentary information to be used in all aforementioned assessment procedures.

**Assessment levels**

For each procedure, there are three possible levels of assessment:

- Level 1: Use conservative procedures with minimal information from inspection and equipment data.
- Level 2: Yields more detailed and less conservative results, compared to those obtained by Level 1. The amount of

information needed to obtain the results is similar to Level 1, however, the calculations are more detailed.

- Level 3: More detailed procedures that yield less-conservative results than those obtained by Level 2, based on numerical analysis (finite element method, for example).

The assessment methodology is comprised of 8 steps and reference 11 has an excellent summary of them, which is replicated below.

1. Flaw and damage mechanism identification: The first step in a FFS assessment is to identify the flaw type and cause of damage. FFS assessments should not be performed unless the cause of the damage can be identified. The original design and fabrication practices, materials of construction, service history, and environmental conditions can be used to ascertain the likely cause of the damage. Once the flaw type is identified, the appropriate section of this document can be selected for the assessment
2. Applicability and limitations of the FFS assessment procedures: The applicability and limitations of the assessment procedure are described in each section, and a decision on whether to proceed with an assessment can be made.
3. Data requirements: The data required for FFS assessments depend on the flaw type or damage mechanism being evaluated. Data requirements may include: original equipment design data; information pertaining to maintenance and operational history; expected future service; and data specific to the FFS assessment such as flaw size, state of stress in the component at the location of the flaw, and material properties. Data requirements common to all FFS assessment procedures

are covered in Section 1. Data requirements specific to a damage mechanism or flaw type are covered in the section containing the corresponding assessment procedures

4. Assessment techniques and acceptance criteria: Assessment techniques and acceptance criteria are provided in each section. If multiple damage mechanisms are present, more than one section may have to be used for the evaluation.
5. Remaining life evaluation: An estimate of the remaining life or limiting flaw size should be made. The remaining life is established using the FFS assessment procedures with an estimate of future damage rate (i.e. corrosion allowance). The remaining life can be used in conjunction with an inspection code to establish an inspection interval.
6. Remediation: Remediation methods are provided in each section based on the damage mechanism or flaw type. In some cases, remediation techniques may be used to control future damage associated with flaw growth and/or material degradation.
7. In-service monitoring: Methods for in-service monitoring are provided in each section based on the damage mechanism or flaw type. In-service monitoring may be used for those cases where, a remaining life and inspection interval cannot be adequately established because of the complexities associated damage mechanism and service environment.
8. Documentation: The documentation of an FFS assessment should include a record of all data and decisions made in each of the previous steps to qualify the component for continued operation. Documentation requirements common to all FFS assessment procedures are given in Section 2 of API 579. Specific documentation requirements for a particular damage mechanism or flaw type are covered in the section containing the corresponding assessment procedures<sup>11</sup>.”

The API 579 is a very detailed, comprehensive, and voluminous standard (over one thousand pages in the 2007 edition) that makes any attempt to review it in detail likely to be countered with word-count restrictions. To get a better understating of how a typical analysis is done, it is simplest to explore one example of a valve-related assessment.

**Example of API 579 assessment**

This example takes us back to the Badak LNG plant and a steam valve displaying several cracks. The valve was a 22-years-old 24” #600 flexible gate valve, build in ASTM A217

Table 1: Overview of Flaw and Damage Assessment Procedures (API 579).	
Flaw or Damage Mechanism	API 579 Part
Brittle Fracture	3
General Metal Loss	4
Local Metal Loss	5
Pitting Corrosion	6
Blisters and HIC/SOHIC Damage	7
Weld Misalignment and Shell Distortions	8
Crack-Like Flaws	9
High Temperature Operation and Creep	10
Fire Damage	11
Dent, Gouge, and Dent Gouge Combinations	12
Laminations	13

WC6 and operating at 450 °C (842 °F) and 62 kgf/cm<sup>2</sup> (882 Psig). Figure 2 shows the overall appearance of the cracks.

The first step in a FFS assessment is flaw characterization. In this case, the cracks were sized with Alternating Current Potential Drop (ACPD). Material properties could not be directly retrieved from the valve, so it was decided to use test specimens from a discarded valve (same grade material and foundry). Testing on the specimens included chemical analysis, tensile testing (room and elevated temperature), fracture toughness (CTOD) testing, and fatigue crack growth testing. The latter was included because of the assumption regarding what mechanism originated the cracks - fatigue induced by cyclic variations of temperature and pressure during operation.

### Finite Element model

Following the flaw and materials characterization, the next step in the analysis was to create an accurate Finite Element model of valve body and bonnet. The model permitted the operator to study the stress distribution

at the crack locations, and thus provide the stress values required as input data to the fitness-for-service assessment.

Given the nature of the flaw, it was decided to conduct a level 3 assessment according to Part 9 of the API 579 (Crack-like flaws). In such cases, the tool that is used to decide whether it is safe or not to continue operation is the Failure Assessment Diagram, or FAD. The FAD is a graph where the vertical axis indicates the resistance of the structure to brittle fracture, and the horizontal axis assesses its resistance to plastic collapse. "In a FFS analysis of crack-like flaws, the results from a stress analysis, stress intensity factor and limit load solutions, the material strength, and fracture toughness are combined to calculate a toughness ratio, Kr, and load ratio, Lr. These two quantities represent the coordinates of a point that is plotted on a two-dimensional FAD to determine acceptability. If the assessment point is on or below the FAD curve, the component is suitable for continued operation?" Figure 3 shows an example of a FAD developed for the bonnet.

### Conclusion

The final results for the assessment stated that the cracks located both on body and bonnet were not likely to grow if temperature cycling was limited and operating temperature decreased. The valve remained then in operation, under these restricted conditions, until a new valve could be procured. The author's final remark is that "...it is recommended to perform crack monitoring to confirm that there is no crack extension using ACPD<sup>12</sup>."

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Figure 2: Cracks observed on the valve<sup>12</sup>.

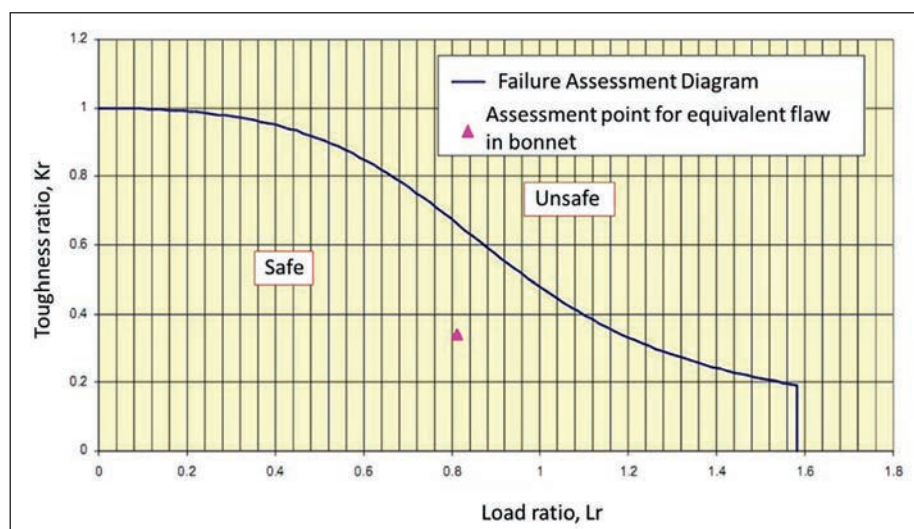


Figure 3: Location of failure assessment point for flaw in valve bonnet<sup>12</sup>.